

Introduction:

This spreadsheet system is an attempt to provide a new kind of learning tool. It is intended, clearly, to be a working link model in order to allow satellite system designes to design and then document fully the Fif radio links associated with Command (uniform) and Telemetry (downtins) equapment. It is, however, also intended to be a butfort on the Fig Portion of a satellite system. The mode does latellite after the Fig Portion of a satellite system. The mode does latellite she trail used Fig Portion days and the value of the sate latellite after the undestanding (and hopefully the fixed for the fixed kinded Operator (fixed Fixed Fixe

Instructions for Use:

Colors are used in the link model to make it easier to find data and to protect the link model from crashing. Many of the worksheets are interconnected in that equations in nor Will Serie forward or back to data located in other worksheets. Loss of this connection could be critical. Also, the cells are not per protected (and may never be) as the system has not yet been finalized. Color can be used to provide "confer" messages the link model operator's brain, once it has been used for awhite. This has been found by the designer to be flashy effective (at least with his brain). Color is used to both the lot and the cell background. Some colors have been plotted for tage feel areas where it is not so in either to have the Least of grid structure showing. Typically, light pay.

If you may be compared to the color of the cell of the product of the product of the product of the series of the cells of the product o

he have been found by our staff psychologist to have a relaxing effect on the operator. Now left slock at the important uses of coor.

"Section 1 in a 1-pour hor relax or will see a left of single-one throughout neuronic and text doll limits." Living your rounce, glace-year cursor on the call. You don't need to citic. A hold will pop up. These are either local instructions on hors to release date or use the contract on the call. You don't need to citic. A hold will pop up. These are either local instructions on hors to release date or use the contract of the call of the contract on the call of the c

XXX. This is a data entry cell. The link model operator is expected to enter data. The blue background means it is a critical data entry cell. It is articipated that your system's selected value is quite likely to be different than the default value used in the cell when you received this link not.

XXX This is also a data entry cell. This type of cell may not need to be changed as the value you are likely to use may be the same as the default value.

XXX This is a cell containing an equation or a constant that should not be changed. The operator should not modify these cells. A majority of the link model contains this type of cell.

XXX or XXX These are cells containing important but, intermediate results. Two colors were used to provide a slight gradation of importance. The orange color is considered to be a result having slightly more significance than the lighter yellow cell.

XXX This is a key "bottom line" result. It is a primary output of a particular W/S.

X or X or X or X A few cells use conditional formatting which allow the cell colers to change depending on the outcome of the preceeding calculations. Typically a RED box means the result was not successful in achieving the desired performance. A A GREEN box means the result achieved the performance threshould but, so considered marginal.

Sub-Title Box A pink box like this is simply a sub-title for a sub-worksheet.

XXX An offive green box is a location where data has been transferred to this worksheet from another and may be transferred to yet another. No action need be taken here. It's purpose is only so that the operator is aware that the data is being transferred from and to other locations.

Frequency Sometimes an ofive green cell will be used to re-emphasize a frequency selection as in the "System Performance Summary" W/S.

Non-Coherent FSK Sometimes a tan color cell is used to denote a selected system condition that is non-numeric.

Gains and Losses:

A positive gain or directivity is always expensed as a positive number. Sometimes the value may be seen to have a * in front of it.

Gains can also be negative (remember, the gain of an antenna is expressed as 100g(P)Pisatopol). So, if the gain in a particular direction, is below that of an isotropic radiation, hen the gain will be expressed as a negative number in 60.

Losses in link budgets are commonly found as either positive or negative. A loss, by it's nature, is a negative quantity but, some believe that if this ideality referred to as such in the budget parameter column, it can have a positive agor. That is the case in this link budget. All bases are show as their jap positive value. The argument is symmitte. The question could be asked, "Is a positive saw pregister" and is a negative loss, positive has been produced thing for the link model cases to know when using this modeling system is that the bases are activated any positive values BUT, in the case in the pairs and tobes to liyed the result, the gains are added and the bases are authorised. For example, we see the equation in Cell [811] of the "Upin's Wis."

Speciality WiS vs. Tools:

The first 13 W/Ss are all interconnected, in that they all have equations that make use of data contained in one or more of the other W/Ss. These worshareds, taken together, constitute the link model. The next 5 W/Ss are supplement to the model and are considered to be too. The important distinction is, that tools exerp produce results that are automatically inked into the model itself, whereas within the first 13 W/Ss there is lots of interfixing going on. The primary process is one where data calculated or selected in one of the Specialty W/Ss (e.g. "Receivers") becomes just one entry in either the liphin or the Downlink budget. The usefulness of a tool is to be able to explore a specific tradeoif without having to worry about that data winding up in the formal Uprin or Downlink fagges.

There is one additional and imporatant comment about tools. Within the Speciality W/Ss, there are some embedded tools. The best example of this is in the "Receivers" W/S. Contained in separate sub-tables is a Notee Figure/Noise Temperature Calculator (Tool) and a Ground Station. Antenior or SN Wholes Temperature Calculator Tool.

Proceeding Through the Modet

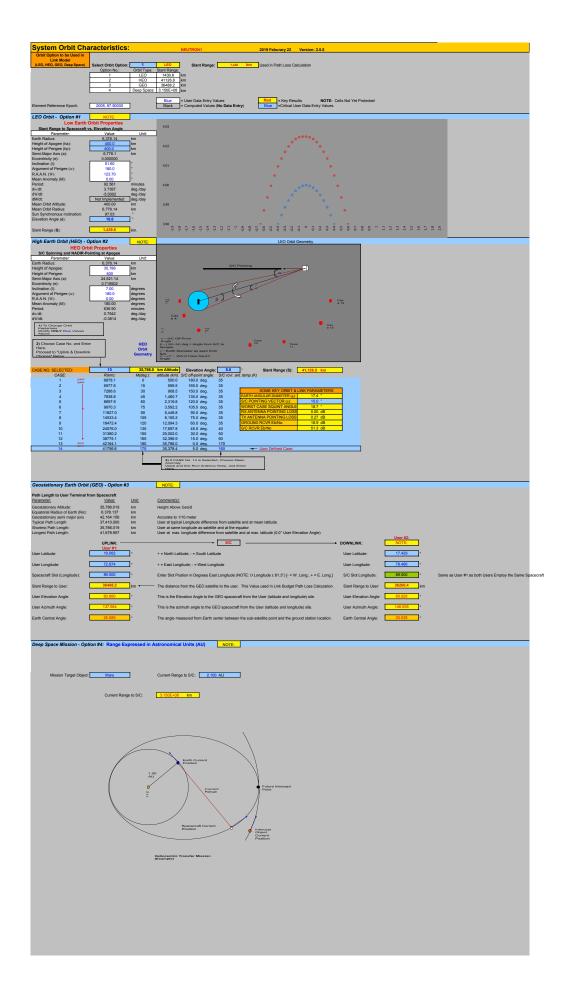
Starting with the "Title Page" WIS, proceed through each Speciality WIS, adding data, in sequence. Then select the next bit at the bottom of the WIS. The "Upinis", "Downlink" and "System Performance Summary" WISs accordant her final results of the modet. The Took WISs are located be proof the "System Performance Summary" WIS and may be explored and used as they may be helpful to you. Any comments you may have on this model will be greatfully received by me. Thanks!

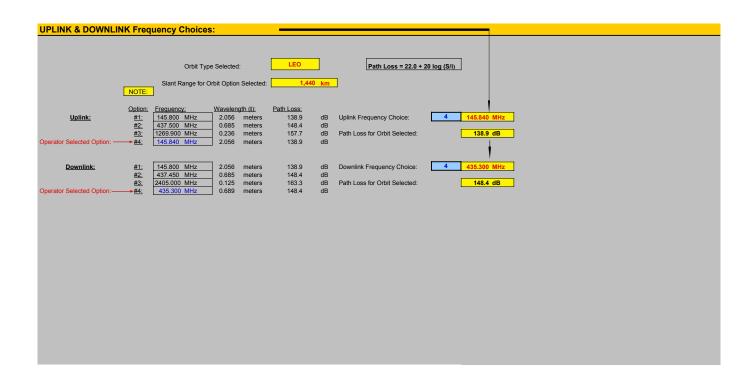
References: The following references were used to prepare this link mo

- 1 A.R.R.L., The ARRL Antenna Handbook, American Radio Relay League, 1974, pp. 153-155.
- Deloraine, E.M., Westman, H.P., Edie, L.C. Reference Data for Radio Engineers, 3rd Edition, Federal Telephone & Radio Corp., 1949, pp. 362-396.
- Feher, Dr. Kamilo, Digital Communications, Satellite/Earth Station Engineering, Prentice-Hall Books, 1983, Chapter 4. Ippolito, L.J.Jr., Radiowave Propagation in Satellite Communications, Van Norstrand Reinhold Co., 1986, Chapters 3 and 7.
- Jordan, E.C. (Edit.), Reference Data for Engineers: Radio, Electronics, Computer, and Communications, 7th Edition, Howard W. Sams & Co., 1985, pp. 29-26 29-37 and pp. 30-03 30-11. Martin, W.L., AMMOS and DSN Support of Earth Orbiting and Deep Space Missions, Jet Propulsion Laboratory, TMOD Directorate, 1996, p.44-46.
- Morgan, W.L. and Gordon, G.D., Principles of Communications Satellites, John Wiley & Sons, Inc., 1993, Chapter 2 and pp.140-143.
- 8 Van Wie, D.G. and Roark, R.C., A New Alert Protocol, Blue Water Design, LLC, 2003, pp. 18-23.
- 9 Jackson, R.B., The Canted Turnstile as an Omnidirectional Spacecraft Antenna, X-712-67-441, NASA/Goddard Space Flight Center, 1967, Entire Documents

Revisions: The following formal revisons have been made to this Link Model System

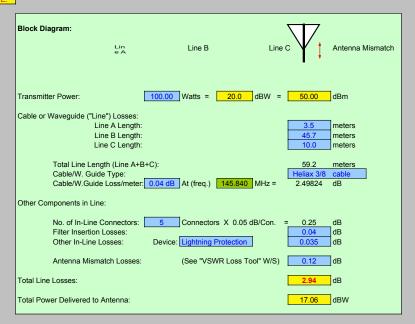
Version:	Date:	Adjustments and/or Modifications Made:
2.0	1/30/2005	NEW; b-Test Version
2.1	2/7/2005	Revised All "Pop-up" Notes; Corrected some cell colors to improve consistancy; Added reference 9; Corrected cells A19 & D19 in "Uplink" W/S.
2.1.1	2/12/2005	Revised Equation at Cell [B15] of "Uplink Budget" W/S. Index function should use column H values not column C values.
2.1.2	2/21/2005	Modified Data for Monopole Antenna Pattern in Monopole Table in "Antenna Patterns" W/S. Added 3 dB to all Values (0" to 90")
2.1.3	2/26/2005	Modified "Receviers" W/S. Added loss value for cable D. Modified 2nd Stage to "Communications Receiver" at Ground Station.
2.1.4	2/27/2005	Added Tubo Code Option to "Modulation-Demodulation Method" W/S.
2.2	2/27/2005	Added EZNEC+ and Chart Wizzard Antenna Plots to "Antenna Pattern" W/S.
2.2.1	5/15/2005	Edited Notes in LLR.R W/S.
2.2.2	6/23/2005	Edited More Notes Throughout Link Model.
2.3	7/16/2005	Revised Antenna Gain and Antenna Pointing Losses W/Ss to Include a High Gain (Parabolic Reflector) S/C Antenna Option & Iso. Radiator Option.
2.3.1	9/28/2005	Modified Notes at Cells [P135] and [V52] of "Receivers" W/S. Added To reference temperature "readout" at Cell [U56] of "Receivers" W/S.
2.3.2	10/4/2005	Modified Equation at Q62 of "Antenna Gain" W/S. Equation was "=21/(F55/1000)"H62" and now is "=21/((F55/1000)"H62)." TNX Ignacio Mas.
2.4	10/22/2006	Changed "Downlink" to "Uplink" at D22 in "Antenna Gain" W/S. Changed hard coded cells in "Ant. Pointing Losses" W/S for referenced cells. Fixed errors in downlink portion of worksheet. There were several incorrect references. Added Ni
2.5	Not Released	Added HEO, GEO and Deep Space Orbit Capability. Link Model Operator selects options. Separted Orbit and Frequency into two separate pages.
2.5.1	3/6/2008	Repaird Bugs in User #2, Delta Longitude, Range, Azimuth and Earth Central Angle; Thank to Michelle Denise, WSNYV
2.5.2	3/18/2008	Repaired Import of Frequency Values to "Transmitters" and "Receivers" Worksheets; Thanks to Michelle Denise, W5NYV
2.5.3	12/17/2008	In "Atmos. & Ionos. Losses" W/S; temporarily made Atmos. Loss dependent on Manually Set Elevation Angle. This needs more work.
2.5.4	3/11/2014	Revised Beam Roll-off Tool Tab to Include Dish Diameter in Wavelengths and Test for 10 wavelength condition.
2.5.5	10/20/2016	Revised Antenna Polarization Loss (R = 10^(ARi20); Antenna Pointling Loss, Downlink, Ground Station Table: Antenna Gains Corrected; TNX to Kelby Davis, AD7VO



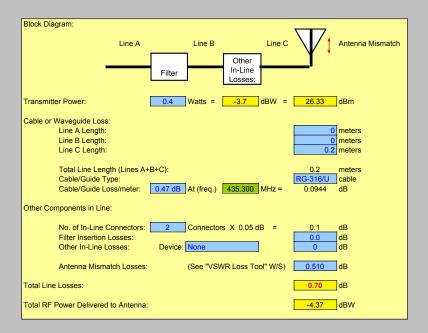


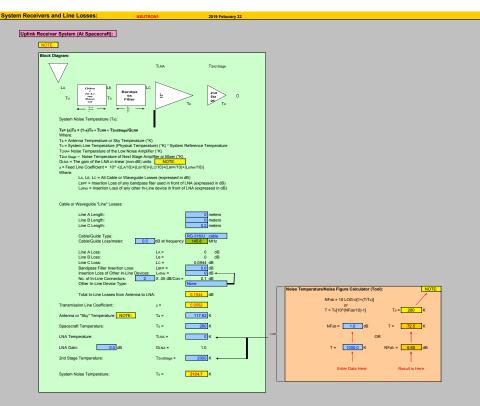
Uplink Transmitter System (At Ground Station):

NOTE:

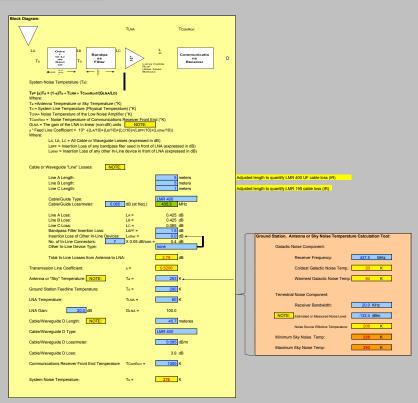


Downlink Transmitter System (At Spacecraft):



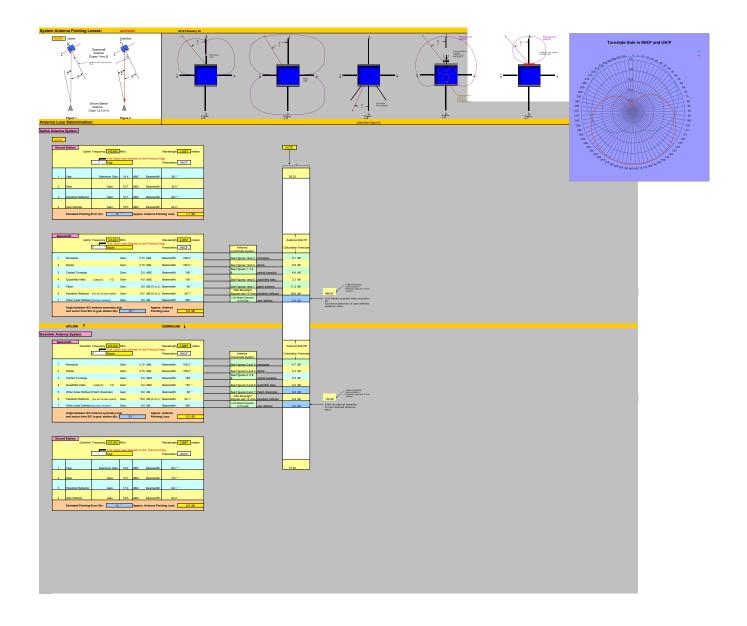


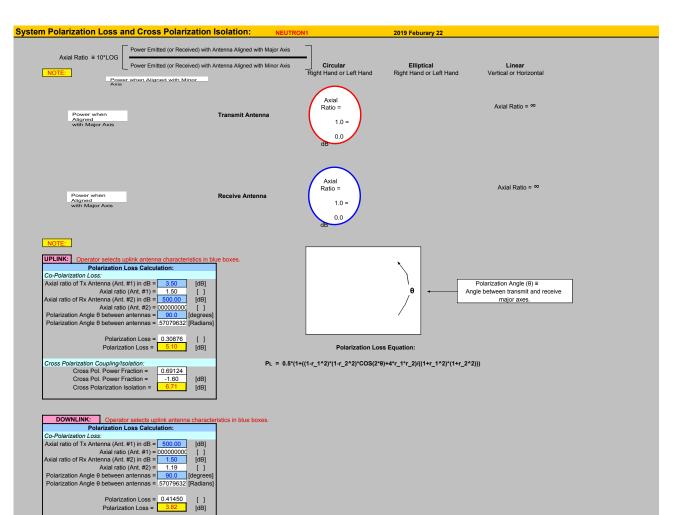
Downlink Receiver System (At Ground Station):





Data Taken from ARRL Antenna Book





	Example Calculations:				
	Tx Ant. A.R. #1: (dB)	Rx Ant. A.R. #2: (dB)	θ (degrees)	Pol. Loss (dB)	
Tx Circular,	0.0	0.0	90.0	0.00	
Rx Variable:	0.0	1.0	90.0	-0.01	
TX Variable.	0.0	2.0	90.0	-0.06	
	0.0	3.0	90.0	-0.13	
	0.0	6.0	90.0	-0.45	
	0.0	10.0	90.0	-1.04	
	0.0	30.0	90.0	-2.74	
	0.0	30.0	0.0	-2.74	
Tx & Rx Elliptical:	3.0	3.0	0.0	0.00	
	3.0	3.0	45.0	-0.25	
	3.0	3.0	90.0	-0.51	
Tx & Rx Linear:	30.0	30.0	0.0	0.00	
	30.0	30.0	30.0	-1.24	
	30.0	30.0	45.0	-2.99	
	30.0	30.0	60.0	-5.97	
	30.0	30.0	90.0	-23.99	
	-				
Tx Elliptical,	2.0	30.0	0.0	-1.91	
Rx Linear	2.0	30.0	45.0	-2.75	
	2.0	30.0	90.0	-3.79	

 Cross Polarization Coupling/Isolation:
 0.58550

 Cross Pol. Power Fraction = Cross Polarization Isolation =
 0.58550

 -2.32
 6.15

Atmospheric and Ionospheric Losses:

NEUTRON1

2019 Feburary 22

Link Losses Resulting from Signals Passing Through Atmospheric Gases:

oss due to Atmospheric Gases Uplink and Downlink:

Elevation Angle: Unit: dB 2.5 ° 4.6 dB 5 ° 2.1 dB 10 ° dB 1.1 30 ° 0.4 dB 45 ° 0.3 dB 90 ° 0.0 dB Min. Elev. Angle: deg.

Losses due to atmospheric gases (Nitrogen, Oxygen, Carbon Dioxide, Hydrogen, etc.) are nearly independent of atmospheric temperature, mean density and relative humidity at frequencies below 2 GHz. Atmospheric absorption depends strongly upon the total number of molecules distincted along the path between the spacecraft and the ground station. This, in turn, means that the losses from or to the satellite are elevation angle dependent.

The table to the left is a look-up table. The minimum elevation angle selected in the "Orbit" worksheet is matched against the closest fit from the table and the result is given at Cell [D23] and is automatically inserted into the uplink and downlink budgets.

The data used here is taken from "Radiowave Propagation in Satellite Communications" by Louis J. Ippolito, Jr., Van Nostrand-Reinhold, 1986, pp. 33-34, Tables 3-3a-c.

One additional interpolated value is added at 2.5° elevation angle. This was not taken from lppolito's text.

If you are using uplink or downlink frequencies above 2 GHz, refer to the referenced text given above to determine the appropriate atmosperic losses. At millimeter wave frequencies the losses can be much higher.

Loss due to Ionosphere: Uplink: Loss Determined: 0.4 dB Frequency: Unit: Loss: Unit: 146 MHz 0.7 dB 438 MHz 0.4 dB 2410 MHz 0.1 dB 0.4 dB 145.840 MHz 0.4 dB 0.4 dB

Loss Determined:

dB

Link Losses Resulting from Signals Passing Through the lonosphere:

Radio waves passing through the ionosphere at VHF, UHF and Microwave frequencies are influenced far less by this layer of ionized particles than at frequencies in the HF, MF and LF portions of the radio spectrum. While there is certainly some correlation between the elevation angle to a satellite and the signal absorption or scintillation experienced, this dependency is nearly masked out by the time variability of effects.

There is, however, a frequency dependency that can be quantified, on average. As transmitter frequencies go below 100 MHz there are times when the attenuation can increase to as much as tens of dB, especially at low elevation angles. The ionosphere certainly limits the lowest frequency at which satellite communications is feasible. Below 20 MHz, during solar maximum space signals are usually fully absorbed or reflected by the layers of the ionosphere (D, E, F1 and F2).

The values provided in this table are approximate mean values for low earth station elevation angles. It is proposed that these values can be conservatively used in satellite link analyses. The higher order statistics of these loss parameters would be interesting to review, however, this effort is more than is necessary for the development of an effective link budget.

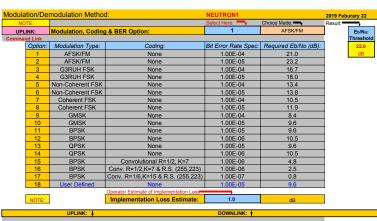
The losses determined here for the uplink and downlink are based on the operator-selected frequency choice made in the "Orbit" worksheet. If the "User Defined" option is selected by the link model operator, then the operator must estimate the appropriate ionospheric loss value and manually insert it in either Cell [D34] or Cell [D47] accordingly.

Link Model Operator Estimate Inserted Here.

Loss due to Ionosphere:								
Downlink:	Loss De	etermined	0.8 dB					
Frequency:	Unit:	Loss:	Unit:					
146	MHz	0.7	dB					
438	MHz	0.4	dB					
2410	MHz	0.1	dB					
435.300	MHz	0.8	dB					
†								

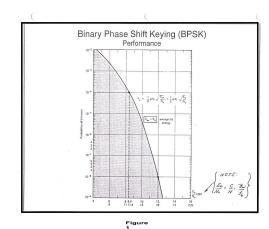
Proceed to the "Modulation-Demodulation Method" W/S

Link Model Operator Estimate Inserted Here. If the "Link Model Operator" has selected a user option for the frequency, then an estimate of the ionospheric losses must be provided by the operator.



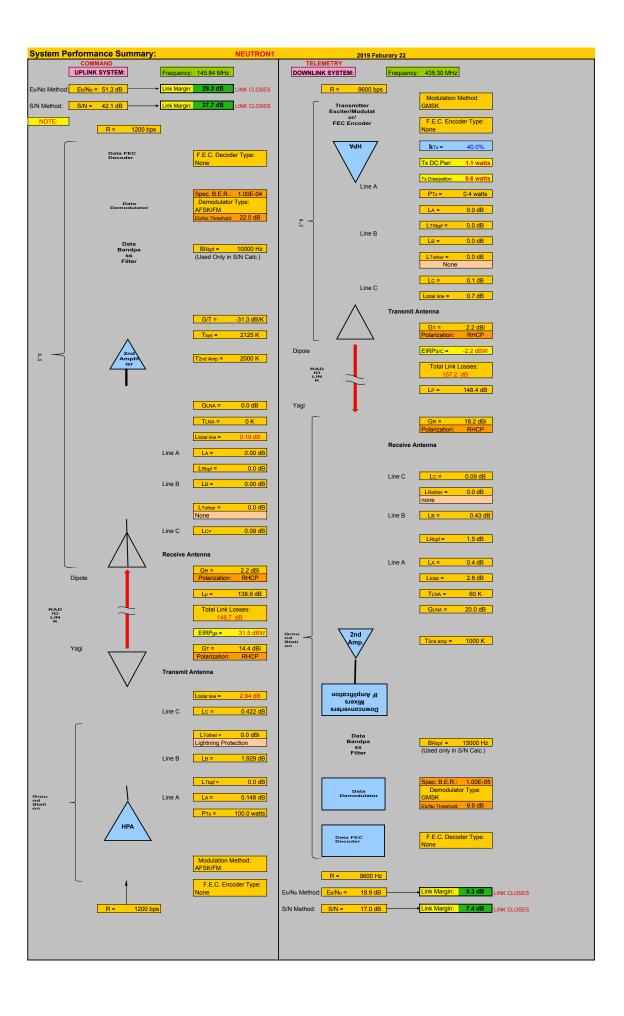
				Select Here:	Choice Made:	ı
DOWNL	INK:	Modulation, Coding & BER Option:		10	GMSK	1
Telemetry	y Link:					Ī
	Option: Modulation Type:		Coding:	Bit Error Rate Spec:	Required Eb/No (dB):	ĺ
	1	AFSK/FM	None	1.00E-04	21.0	1
	2	AFSK/FM	None	1.00E-05	23.2	1
	3	G3RUH FSK	None	1.00E-04	16.7	1
	4	G3RUH FSK	None	1.00E-05	18.0	1
	5	Non-Coherent FSK	None	1.00E-04	13.4	1
	6	Non-Coherent FSK	None	1.00E-05	13.8	1
	7	Coherent FSK	None	1.00E-04	10.5	1
	8	Coherent FSK	None	1.00E-05	11.9	1
	9	GMSK	None	1.00E-04	8.4	Ī
	10	GMSK	None	1.00E-05	9.6	1
	11	BPSK	None	1.00E-05	9.6	1
	12	BPSK	None	1.00E-06	10.5	1
	13	QPSK	None	1.00E-05	9.6	1
	14	QPSK	None	1.00E-06	10.5	1
	15	BPSK	Convolutional R=1/2, K=7	1.00E-06	4.8	1
	16	BPSK	Conv. R=1/2,K=7 & R.S. (255,223)	1.00E-06	2.5	1
	17	BPSK	Conv. R=1/6,K=15 & R.S. (255,223)	1.00E-07	0.8	1
	18	BPSK	Turbo Code (Parallel w. Interleaver)	1.00E-06	0.75	Ī
	19	User Defined	None	1.00E-05	9.6	1
_			Operator Estimate of Implementation Loss			Ī
_			Implementation Loss Estimate:	0.0	dB	

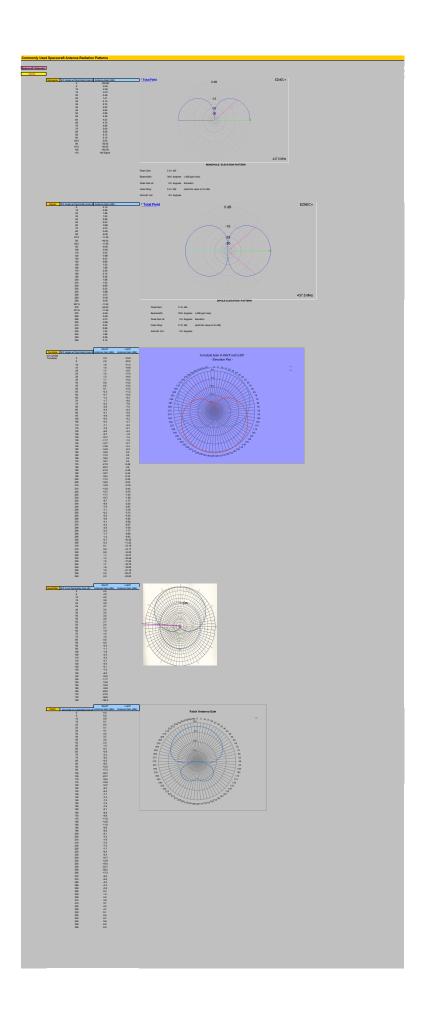
NOTE:



NEUTRON1	NOTE:	NEUTRON1	Date Data Last Modified:	
Uplink Command Budget:		Version: 2.5.5	2019 Feburary 22	
Parameter:	Value: Un	its: Comments:		
Ground Station:				
Ground Station Transmitter Power Output:	100.0 watts	This value is transferred fro	m "Transmitters" W/S, Cell [E15].	NOTE: Click " + " above column J to restore comment column.
In dBW				
In dBn		Transmitter power expresse		
Ground Stn. Total Transmission Line Losses:	2.9 dB		m "Transmitters" W/S, Cell [133]	
Antenna Gain:	14.4 dBi	This value is selected at "Ar	ntenna Gain" W/S, Cell [E11]	
Ground Station EIRP: Uplink Path:	31.5 dBW	Ground Station Effective Iso	otropic Radiated Power (EIRP) [EIRP=Pt x Ltl x Ga]	
Ground Station Antenna Pointing Loss:	1.1 dB	This return is anterdated in the	ne "Antenna Pointing Losses" W/S. and transferred from Cell (K43)	
Gnd-to-S/C Antenna Polarization Losses:	1.1 dB 5.1 dB		ne "Polarization Loss" W/S and is transferred from Cell [F40].	
Path Loss:	138.9 dB		sferred from "Frequency" W/S	
Atmospheric Losses:	1.1 dB		m "Atmos. & Ionos. Losses" W/S, Cell [D23]	
Ionospheric Losses:	0.4 dB		m "Atmos. & Ionos. Losses" W/S, Cell [D47:D50]	
Rain Losses:	0.0_dB		ated by the link model operator and place into Cell [B18]	
Isotropic Signal Level at Spacecraft:	-115.2 dBW	This is the signal level recei	ved in space in the vacinity of the spacecraft using an omnidirectional antenna.	
Spacecraft (Eb/No Method):				
Eb/No Method				
Spacecraft Antenna Pointing Loss:	0.0 dB		m "Antenna Pointing Losses" W/S, Cell [K63]	
Spacecraft Antenna Gain: Spacecraft Total Transmission Line Losses:	2.2 dBi 0.2 dB		ntenna Gain" W/S, Cell [E24] m the "Receivers" W/S, Cell [J52]	
Spacecraft Total Transmission Line Losses: Spacecraft Effective Noise Temperature:	0.2 dB 2125 K		m the "Receivers" W/S, Cell [J52] ne "Receivers" W/S and Transferred from Cell [J67]	
Spacecraft Figure of Merrit (G/T):	-31.3 dB/K		s is the uptimate measure of the receiver's performance.	
S/C Signal-to-Noise Power Density (S/No):	82.1 dBH:		-228.6 dBW/K/Hz	
System Desired Data Rate:	1200 bps		Be Careful! This is the data rate, not the symbol rate.	
In dBH	: 30.8 dBH:	This is simply = 10log(R); R	= data rate	
Command System Eb/No:	51.3 dB			
Demodulation Method Seleted:	AFSK/FM	Values selected in "Modulat	tion-Demodulation W/S, Cell [E3]	
Forward Error Correction Coding Used:	None		on-Demodulation" W/S, also Cell [E3]	
System Allowed or Specified Bit-Error-Rate:	1.0E-04	The selected value is transf	erred from the "Modulation-Demodulation W/S, Cells [E6:E23]	
Demodulator Implementation Loss:	1.0 dB	This value is transferred fro	m the "Modulation-Demodulation W/S, Cell[E25]	
Telemetry System Required Eb/No:	21.0 dB	The selected value is transf	erred from the "Modulation-Demodulation W/S, Cells [F6:F23]	
reterries y cystem requires Estre.	21.0 00	The selected value is trained	circo nom tre modulation bemodulation two, outs [1 c.r 20]	
Eb/No Threshold:	22.0 dB	This is the result of the "Mo	dulation-Demodulation" W/S and is transferred from Cell [H32]	
System Link Margin:	29.3 dB			
Spacecraft Alternative Signal Analysis Metho	d (SNR Computation):	- NO	OTE:	
SNR Method				
Spacecraft Antenna Pointing Loss:	0.0 dB		m "Antenna Pointing Losses" W/S, Cell [K63]	
Spacecraft Antenna Gain:	2.2 dBi		ntenna Gain" W/S, Cell [E24]	
Spacecraft Total Transmission Line Losses: Spacecraft Effective Noise Temperature:	0.2 dB 2125 K		m the "Receivers" W/S, Cell [J52] ne "Receivers" W/S and Transferred from Cell [J67]	
Spacecraft Effective Noise Temperature: Spacecraft Figure of Merrit (G/T):	-31.3 dB/K		is the ultimate measure of the receiver's performance.	
Spacecraft rigure of Metrit (G/1).	-51.5 db/h	G/1 = Ga-Lii-10l0g(1s). 11lis	is the diditate measure of the receiver a performance.	
Signal Power at Spacecraft LNA Input:	-113.2 dBW	Ps = Piso+Ga-Lpt-Ltt; This is	the signal power that has arrived at the ground station receiver.	
Spacecraft Receiver Bandwidth:	10,000 Hz	Signal Spectrum Must Pass	Through This Data Filter. NOTE:	
Spacecraft Receiver Noise Power (Pn = kTB)	-155.3 dBW	Pn = K + 10log(Ts) + 10log	B). This is the total noise power arriving at the ground station receiver.	
Signal-to-Noise Power Ratio at G.S. Rcvr:	42.1 dB	Ps/Pn = Ps(in dBW) - Pn(in	dBW)	
Analog or Digital System Required S/N:	14.4 dB	If system is digital, use valu	es from "Modulation-Demodulation" W/S. If analog, use appropriate value from text book	k
System Link Margin	27.7 dB			

NEUTRON1	NOTE:		NEUTRON1	Date Data Last Modified:	
Downlink Telemetry Budget	:		Version: 2.5.5	2019 Feburary 22	
Parameter:	Value:	Units:	Comments:		
Spacecraft:					
Spacecraft Transmitter Power Output:	0	4 watts	This value is transferred from	"Transmitters" W/S, Cell (E50)	NOTE: Click " + " above column K to restore comment column.
In dBW		dBW	Transmitter power expressed		
In dBm		dBm	Transmitter power expressed		
Spacecraft Total Transmission Line Losses:		7 dB	This value is transferred from		
Spacecraft Antenna Gain:		2 dBi	This value is selected at "Ante		
Spacecraft EIRP:	-22	dBW		Radiated Power (EIRP) [EIRP=Pt x Ltl x Ga]	
Downlink Path:	-2.2	_ ubvv	opacecian Enective isotropic	radiated Fower (Eiror) [Eiror - Frx Eirx Oa]	
Spacecraft Antenna Pointing Loss:	0	3 dB	This value is calculated in the	"Antenna Pointing Losses" W/S, and trasferred from Cell [K85]	
6/C-to-Ground Antenna Polarization Loss:		8 dB		"Polarization Loss" W/S and is transferred from Cell [F60].	
Path Loss:		4 dB			
			Lp = 22 + 20LOG(D/I); Transfe		
Atmospheric Loss:		1 dB		"Atmos. & Ionos. Losses" W/S, Cell [D23]	
onospheric Loss:		8 dB		"Atmos. & Ionos. Losses" W/S, Cell [D47:D50]	
Rain Loss:	0.	0 dB		d by the link model operator and place into Cell [B18]	
sotropic Signal Level at Ground Station:	-156.6	dBW	This is the signal level receive	d at the Earth in the vacinity of the ground station using an omnidirectional antenna.	
Ground Station (EbNo Method): Eb/No Method					
Ground Station Antenna Pointing Loss:		8 dB	This value is transferred from	"Antenna Pointing Losses" W/S, Cell [K102]	
Ground Station Antenna Gain:		2 dBi	This value is selected at "Ante		
Ground Station Total Transmission Line Losses		8 dB		the "Receivers" W/S, Cell [J123]	
Ground Station Effective Noise Temperature:		6 K		"Receivers" W/S and Transferred from Cell [J138]	
Ground Station Figure of Merrit (G/T):		4 dB/K		s the uptimate measure of the receiver's performance.	
G.S. Signal-to-Noise Power Density (S/No):	58.8	dBHz	Boltzman's Constant:	-228.6 dBW/K/Hz	
System Desired Data Rate:	9600	bps		e Careful! This is the data rate, not the symbol rate.	
In dBHz		dBHz	This is simply = 10log(R); R=		
Felemetry System Eb/No for the Downlink:	18.9	dB	This is simply = Tolog(R); R=	data rate	
		_			
Demodulation Method Seleted:	GMSK			n-Demodulation W/S, Cell [E30]	
Forward Error Correction Coding Used:	None		Value selected in "Modulation-	-Demodulation" W/S, also Cell [E30]	
System Allowed or Specified Bit-Error-Rate:	1.0E-05		The selected value is transferr	red from the "Modulation-Demodulation W/S, Cells [E33:E50]	
Demodulator Implementation Loss:	0.0	dB	This value is transferred from	the "Modulation-Demodulation W/S, Cell[E52]	
Telemetry System Required Eb/No:	9.6	dB	The selected value is transferr	red from the "Modulation-Demodulation W/S, Cells [F33:F50]	
Eb/No Threshold:	9.6	dB	This is the result of the "Modul	lation-Demodulation" W/S and is transferred from Cell [H32]	
System Link Margin:	9.3	dB			
Ground Station Alternative Signal Analysis	Method (SNR Co	mputation):			
SNR Method		8 dB	This value is transferred from	"Antonna Bainting Lacase" M/F. Call IV4021	
Ground Station Antenna Pointing Loss:				"Antenna Pointing Losses" W/S, Cell [K102]	
Ground Station Antenna Gain:		2 dBi	This value is selected at "Ante		
Ground Station Total Transmission Line Losses		8 dB		the "Receivers" W/S, Cell [J123]	
Ground Station Effective Noise Temperature: Ground Station Figure of Merrit (G/T):		6 K 4 dB/K		"Receivers" W/S and Transferred from Cell [J138] the ultimate measure of the receiver's performance.	
Signal Power at Ground Station LNA Input:	-144.1	dBW	Ps = Piso+Ga-Lpi-Lti; This is th	e signal power that has arrived at the ground station receiver.	
Ground Station Receiver Bandwidth (B):	15,000	Hz	Signal Spectrum Must Pass Ti	hrough This Data Filter NOTE:	
G.S. Receiver Noise Power (Pn = kTB)	-161.1	dBW	Pn = K + 10log(Ts) + 10log(B)	. This is the total noise power arriving at the ground station receiver.	
Signal-to-Noise Power Ratio at G.S. Rcvr:	17.0	dB	Ps/Pn = Ps(in dBW) - Pn(in dB	BW)	
Analog or Digital System Required S/N:	9.6	dB	If system is digital, use values	from "Modulation-Demodulation" W/S. If analog, use appropriate value from text book.	
System Link Margin	7.4	dB			





"Design a Dish"

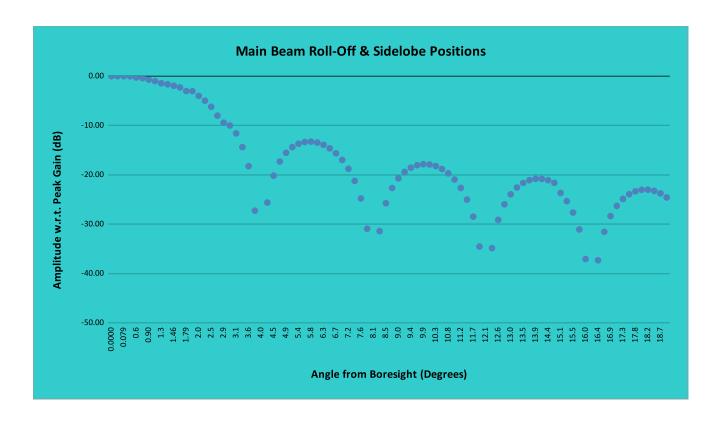
"Design a Dish"
Antenna Beam Roll-Off Tool
Beam Roll-Off & Sidelobe Positions Based on Sin' (9)/ 8" Formulation

Frequency: 2.4 GHz Peak Gain: 33.1 dBl (See Plot at Next Worksheet)
Antenna Dia.: 2.4334 Meters
Antenna Dia.: 2.43354 Meters
55 % Half Power (P/2) Beamwidth: 3.588 * =2q (Beamwidth@ -3dB Roll-Off)

Wavelength: 0.125 m

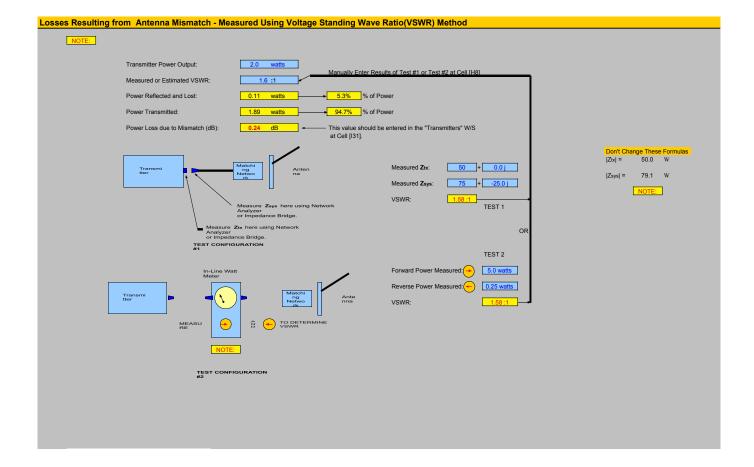
Dish Size?
OK

	NOTE D	Dish D	I- 4- I-6 -64-' '				
NOTE:	NOTE: Do not r	nodify or use cel	Is to left of table.	Pwr (q) w.r.t. Pe	ak Gain:	q (degrees):	
	•		•	0.00		0.0000 Main Lobe	_
				-0.000004		0.002	
				-0.01	dB	0.079	
				-0.04	dB dB	0.225 0.6	
					dB	0.6	
				-0.7	dB	0.90	
				-1.00		1.06	
				-1.5	dB	1.3	
					dB	1.3	
				-2.0	dB	1.46	
				-3.01	dB	1.6 1.79 (Half Power B.)	14/1/2
				-3.03		1.8 (Hall Fower B.)	14.112
				-4.00		2.0	
					dB	2.25	
					dB	2.5	
					dB	2.7 2.9	
				-10.00	dB dB	2.99	
				-11.6		3.1	
				-14.4		3.4	
				-18.2	dB	3.6	
				-27.3		3.880	
				-328.2	dB	4.0 First Null	
				-25.6		4.3	
				-20.2 -17.3		4.5 4.7	
				-15.5		4.9	
				-14.4		5.2	
				-13.7		5.4	
				-13.3		5.6 First Sidelobe	
				-13.3 -13.5		5.8 6.1	
				-13.9		6.3	
				-14.6		6.5	
				-15.6	dB	6.7	
				-17.0		7.0	
				-18.8		7.2	
				-21.2		7.4	
				-24.8 -30.9	dB	7.6 7.9	
				-328.2		8.1 2nd Null	
				-31.4		8.3	
				-25.8		8.5	
				-22.7		8.8	
				-20.7 -19.4		9.0 9.2	
				-18.6		9.4	
				-18.0		9.7	
				-17.8		9.9 2nd Sidelobe	
				-17.9		10.1	
				-18.2		10.3	
				-18.8 -19.7		10.6 10.8	
				-21.0		11.0	
				-22.7		11.2	
				-25.0		11.5	
				-28.5		11.7	
				-34.5		11.9	
				-328.2 -34.9		12.1 3rd Null 12.4	
				-34.9		12.4	
				-26.0		12.8	
				-23.9	dB	13.0	
				-22.6	dB	13.3	
				-21.6		13.5	
				-21.1		13.7	
				-20.8 -20.8		13.9 3rd Sidelobe 14.2	
				-20.8 -21.1		14.2	
				-21.6		14.6	
				-23.7	dB	15.1	
				-25.3	dB	15.3	
				-27.6		15.5	
				-31.1 -37.1		15.7	
				-37.1		16.0 16.2 4th Null	
				-328.2 -37.3	dB	16.4	
				-31.5		16.6	
				-28.4	dB	16.9	
				-26.3	dB	17.1	
				-24.9		17.3	
				-23.9	dB	17.5	
				-23.3 -23.0		17.8 18.0	
				-23.0		18.0 18.2 4th Sidelobe	
				-23.2		18.4	
				-23.8	dB	18.7	
				-24.6	ав	18.9	

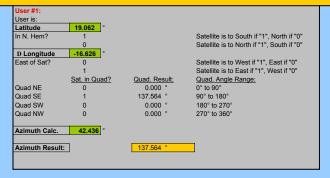


| RG-142 AU: An FEP (Teffon) solid covered "clean" cable for general purpose spacecraft transmission lines.
| Losses are moderate per unit length as the cable clameter is 0.165" (4.95 mm). The losses are quite acceptable even solid copen AVIG #18. "Strange and the cable clameter is 0.165" (4.95 mm). The losses are quite acceptable even solid copen AVIG #18. "Strange length and the control of the solid copen AVIG #18. "Strange length and the cable length and the cable

| RG-303 | U: A PTFE (Teflon) solid covered "clean" cable for ruggedized spacecraft transmission line applications.
| Losses are moderate per unit length as the cable dismeter is 0.170" (4.32 mm). The losses are quite acceptable even for longer SC cable units. The cable is night except to share the cable of the shedded with a share coated copper braid. The center conductor is share over topper over steel 0.050" (1 mm) dis. Typically used with SMA or even TNC connections. This is a very rugged cable type | Band | 1 mm | 1



GEO Azimuth Calculation:





Earth and Orbit Shape for Figure in Orbit & Frequency W/S [NOTE: DO NOT MODIFY]

Earth and Orbit Shape fo				
NOTE: Y .51994318	X -1.9	R Y1 163.57456291	X1 -1.9	R1 16.2
.54647712	-1.85	16 3.6	-1.85	16.2
3.57211422	-1.8	163.62456894	-1.8	16.2
.59687364	-1.75	16 .64828726	-1.75	16.2
.62077339	-1.7	16 .67117147	-1.7	16.2
.64383040 .66606055	-1.65 -1.6	16 .69323706 16 3.71449862	-1.65 -1.6	16.2 16.2
.68747881	-1.55	16 .73496987	-1.55	16.2
.70809924	-1.5	16 .75466376	-1.5	16.2
.72793508	-1.45	16 .77359245	-1.45	16.2
.74699879	-1.4 1.25	16 .79176739	-1.4 -1.35	16.2
.76530211 .78285606	-1.35 -1.3	16 .80919939 16 .82589858	-1.35	16.2 16.2
.79967103	-1.25	16 .84187454	-1.25	16.2
.81575680	-1.2	16 .85713624	-1.2	16.2
.83112255	-1.15	16 .87169213	-1.15	16.2
.84577690 3.85972797	-1.1 -1.05	16 .88555015 16 .89871773	-1.1 -1.05	16.2 16.2
.87298334	-1.05 -1	16 .91120186	-1.05	16.2
.88555015	-0.95	16 .92300904	-0.95	16.2
.89743505	-0.9	16 .93414539	-0.9	16.2
.90864426	-0.85	16 .94461658	-0.85	16.2
.91918358 .92905841	-0.8 -0.75	16 .95442789 16 .96358423	-0.8 -0.75	16.2 16.2
.93827373	-0.7	163.97209013	-0.73	16.2
.94683417	-0.65	16 3.979950	-0.65	16.2
.95474398	-0.6	16 .98716691	-0.6	16.2
.96200706	-0.55	163.99374511	-0.55	16.2
.96862696	-0.5 -0.45	16 .99968748 16 .00499687	-0.5 -0.45	16.2 16.2
.97994974	-0.4	16 .00967579	-0.43	16.2
.98465807	-0.35	16 .01372644	-0.35	16.2
.98873413	-0.3	16 .01715073	-0.3	16.2
.99217985	-0.25	16 .01995024	-0.25	16.2
.99499687 .99718651	-0.2 -0.15	16 .02212630 16 .02367990	-0.2 -0.15	16.2 16.2
.99874980	-0.1	16 .02461178	-0.1	16.2
.99968748	-0.05	16 .02492235	-0.05	16.2
4.000000	0	16 4.0249223	0	
3.99968748 3.9987498(0.05 0.1	16 4.02461178 16 4.02367990	0.05 0.1	16.2 16.2
3.9971865	0.15	16 4.02212630	0.15	16.2
3.99499687	0.2	16 4.01995024	0.2	16.2
3.9921798	0.25	16 4.0171507:	0.25	16.2
3.98873413 3.98465807	0.3 0.35	16 4.0137264 ² 16 4.00967579	0.3 0.35	16.2 16.2
3.97994974	0.4	16 4.00499687	0.4	16.2
3.97460689	0.45	16 3.99968748	0.45	16.2
3.96862696	0.5	16 3.9937451:	0.5	16.2
3.96200706	0.55	16 3.9871669:	0.55	16.2
3.95474398 3.94683417	0.6 0.65	16 3.97994974 16 3.97209013	0.6 0.65	16.2 16.2
3.9382737	0.7	16 3.9635842	0.7	
3.92905841	0.75	16 3.95442789	0.75	
3.91918358	0.8	16 3.94461658	0.8	
3.90864426 3.89743505	0.85	16 3.93414539 16 3.92300904	0.85 0.9	16.2 16.2
3.8855501!	0.9 0.95	16 3.9112018	0.95	16.2
3.87298334	1	16 3.8987177	1	16.2
3.85972797	1.05	16 3.8855501!	1.05	16.2
3.84577690	1.1	16 3.8716921	1.1	16.2
3.8311225! 3.8157568(1.15 1.2	16 3.8571362 ² 16 3.8418745 ²	1.15 1.2	16.2 16.2
3.7996710	1.25	16 3.82589858	1.25	16.2
3.78285606	1.3	16 3.80919939	1.3	
3.76530211	1.35	16 3.79176739	1.35	16.2
3.74699879 3.72793508	1.4 1.45	16 3.7735924! 16 3.75466376	1.4 1.45	16.2 16.2
3.7080992	1.45	16 3.73496987	1.45	16.2
3.6874788	1.55	16 3.71449862	1.55	16.2
3.66606055	1.6	16 3.69323706	1.6	16.2
3.6438304(1.65	16 3.67117147	1.65	16.2
3.62077339 3.59687364	1.7 1.75	16 3.6482872(16 3.6245689 ²	1.7 1.75	16.2 16.2
3.57211422	1.73	16 3.6	1.8	
3.54647712	1.85	16 3.57456291	1.85	16.2
3.51994318	1.9	16 3.548239	1.9	16.2